

K&C Construction Ltd

Ysgol Caerhun, Conway Road

Outline Drainage Strategy





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Outline Drainage Strategy

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1 Introduction

1.1 Appointment

Opus International Consultants (UK) Ltd (OPUS) were commissioned by K&C Construction Ltd in April 2017, to undertake a Drainage Strategy Report in support of a Full Detailed Planning Application for the redevelopment of Dolgarrog Primary School into Ysgol Caerhun.

1.2 Existing Site

The proposed site is situated to the east of Conway Road (B5106), and is centred at NGR 276959, 367960 and a topographical survey of the site is provided within Appendix 4.1. The site covers an area adjacent to Conway Road which is currently occupied by school buildings and associated hardstanding. The northern, western and southern boundaries of the site are formed by undeveloped open fields and the eastern boundary is formed by Conway Road which is also the main point of access to the site.

The site area is 0.78ha, of which 0.462ha is currently hardstanding. The remainder comprises of landscaped areas.

A review of the topographical survey shows that the site generally falls in a south easterly direction, with the highest ground level being around 18.5mAOD at the north-western corner of the site and the lowest point being at 10mAOD near the south-eastern corner of the site.

Sewer records have been obtained from Dwr Cymru Welsh Water (DCWW) for this area. These show the presence of a public combined sewer running along the southern boundary of the site to a public pumping station. The sewer records are shown in Appendix 4.2.

A drainage survey has recently been provided by the Client. This survey has shown that both foul and surface water from the existing buildings (0.13ha) are currently drained via a combined sewer which communicates with the public combined sewer running along the southern boundary of the site. None of the hardstanding areas appear to be positively drained and the surface water run-off from these areas appear to follow the natural topography of the site, draining overland to the southern boundary and beyond. The drainage survey plan is provided in Appendix 4.3

1.3 Existing Flood Risk

In accordance with the Natural Resources Wales (NRW) online Maps (shown in Appendix 4.4), the site is located within Flood Zone A – Land having less than 1 in 1000 annual probability of river or sea flooding.

Due to the topography of the area, the risk of flooding from adjoining properties or roads is considered to be minimal, and therefore, the management of the surface water run-off generated by the post development site will be the principal flood risk associated with this scheme.

1.4 Proposed Development

The scheme consists of the demolition of the existing school buildings and the construction of a new school building, parking and associated hardstanding areas.

Based upon the latest development plans, the final impermeable area generated by the proposals will be approximately 0.402ha.

A copy of the latest proposed development plan is included in Appendix 4.5.

2 Drainage Proposals

2.1 Foul Drainage

The existing school has capacity for 90 pupils and the proposed school will be designed to cater for 120 pupils, therefore, the peak foul discharge will increase marginally following the redevelopment of the school.

It is proposed to drain foul water from the proposed development to the local foul sewer currently serving the site. The foul drainage system is proposed to be designed in accordance with all statutory requirements including Part H1 of Building Regulations 2010 (2015 Edition). It is proposed to reuse the existing connection to the public sewer under a Section 106 Agreement.

Initial discussions are underway with DCWW in respect to the foul discharge and a response is awaited.

2.2 Surface Water Drainage

It is acknowledged that the satisfactory collection, control and discharge of storm water is now a principal planning and design consideration.

Surface water drainage systems are required to consider quantity, quality, amenity and biodiversity whilst preventing any likelihood of flooding to the site or adjacent sites. Part H₃ of the Building Regulations 2010 and surface water management guidance reviewed from Essex County Council recommend that surface water runoff shall discharge to one of the following, listed in order of priority:

- a) an adequate soakaway or some other adequate infiltration system, or where that is not reasonably practicable,
- b) a watercourse, or, where that is not reasonably practicable,
- c) a sewer.

It is necessary to identify the most appropriate method of controlling and discharging surface water. The design should seek to improve the local run-off profile by using systems that can either attenuate run-off and reduce peak flow rates or positively impact on the existing flood profile.

2.2.1 Ground Infiltration Techniques

The following geotechnical desk study was reviewed as part of this assessment:

 Ground Investigation Report, Dolgarrog Primary School, SRL Strata Renewables Ltd, August 2016.

Summary of Ground Conditions:

Macadam surfacing At each borehole, 100mm thick. Sub-base granular fill at BH02 and

BH04 200mm and 300mm thick respectively.

Made Ground Mixed Made Ground of brown sandy gravelly low cobble content Fill.

Much slate gravel.

Thickness in the range 900mm BH01: Absent at BH02 and BH04.

At BHo3 the Made Ground is clay fill of dark grey silty peaty organic CLAY

with wood pieces and sparse angular gravel of slate.

Glacial Clay Firm-stiff brown streaked grey fine-medium fine-coarse subangular and

subrounded sandy gravelly CLAY. Gravel is some of slate.

The clay is of Low Plasticity

There are cobbles in the soils mass which would result in the termination of

the Continuous Dynamic Sample and Continuous Dynamic Sounding.

Where the Standard Penetration Test was completed to full penetration the N300 values were in the range 17-37. Where the Standard Penetration Test was incomplete the results are 55/30mm (BH02) 50/300mm (BH03) and 50/10mm (BH04). The Standard Penetration Test N300 values are presented.

No Groundwater was encountered during the sampling.

It is considered that the site to be poor with soakaway drainage, given the low permeable soils encountered and at this stage the option of using soakaways or infiltration drainage systems has been discounted.

2.2.2 Discharge to Watercourse

A review of the online Ordnance Survey Mapping data has indicated that the nearest open watercourse (Afon Porth-llwyd) is located approximately 250m to the south of the site. Due the distance and local land use, a connection to this watercourse for surface water drainage purposes will neither be cost effective nor feasible without crossing third party land. On this basis this option has been discounted.

2.2.3 Connection to Sewer

In the event that infiltration drainage systems are proved to be unsuitable for the discharge of surface water run-off from the proposed development, the surface water drainage system for the proposed development will have to discharge to a local sewer at a maximum agreed discharge rate.

2.2.3.1 Surface Water Sewer

There are no surface water sewers identified on DCWW public sewer records.

A review of Conway Road has shown that there are no road gullies on the road in close proximity of the site. The nearest road gullies are approx. 225m south, at the point the road crosses the Afon Porth-llwyd, and therefore, it is assumed that there is no Highway Drainage within the vicinity of the site that could be utilised as a point of discharge.

2.2.3.2 Combined Sewer

An existing Public Combined Sewer is situated along the southern boundary of the site to which the site currently drains surface water run-off from the school buildings. Given the close proximity of the combined sewer and that surface water flows from the site currently communicate with the combined sewer, we would advocate that a connection to the combined sewer is pursued.

Initial discussions are underway with DCWW in respect to the surface water flows re-communicating with the combined sewer and a response is awaited.

2.2.4 Allowable Discharge Rate

In the event that infiltration drainage systems are proved to be unsuitable for the discharge of surface water run-off from the proposed development, the surface water drainage system for the proposed development will have to discharge to the local sewers upon a maximum agreed discharge rate. The recent drainage survey has shown that rainwater from the site currently discharges directly into the foul sewer crossing the site without any attenuation.

2.2.4.1 Existing Greenfield Run-off Rate

The existing Greenfield run-off rates for the site have been calculated and are as follows and are attached within Appendix 4.6.

Existing Greenfield Discharge Rates						
Return Period	Existing Discharge Rate (l/s)					
$Q_{ m bar}$	10.3					
1 in 30 year	18.2					
1 in 100 year	22.5					

2.2.4.2 Existing Brownfield Run-off Rate

The allowable discharge rate, from the site may also be estimated by assuming the unrestricted runoff from the existing impermeable areas contributing flows to the public sewer.

Within Section 1.2, we have stated that 0.13 Ha of impermeable area currently contributes surface water flows to the public combined drainage system situated within along the southern boundary of the site.

Therefore, it is possible to estimate the run-off generated by the existing site area for events up to 1 in 100 year years by using the Lloyd-Davies method thus;

$$Q=2.78.A.i.C_vC_r \qquad Where \qquad A \qquad = \quad Area \ (ha)$$

$$I \qquad = \quad Design \ rainfall \ intensity \ (mm/hr)$$

$$C_vC_r \qquad = \quad Run \ off \ \& \ routing \ coefficient \ \sim \ 1.0$$

Allowing for a rainfall intensity of 50mm/hr (1 in 1 Year Storm) with a 30% betterment provided to determine the peak flow from the site and based upon an impermeable area of 0.13 ha, the peak flow generated would be:

$$Q = 2.78.A.i.C_vC_r$$

 $Q = 2.78 \times 0.13 \times 50 \times 1$
 $Q = 18.07 \text{ l/s}$

Applying the 30% betterment requirement, the maximum allowable discharge from the site would be:

$$Q_{max} = Q \times 0.7$$

 $Q_{max} = 18.07 \times 0.7$
 $Q_{max} = 12.65 \text{ l/s.}$

2.2.4.3 Proposed Discharge Rate

Based upon the above, we would advocate that the surface water discharge is limited to the existing Greenfield runoff Q_{bar} rate of 10.3l/s which is achieves a 43% betterment on the existing brownfield discharge.

Initial discussions are underway with DCWW in respect to the surface water discharge and a response is awaited.

2.2.5 Scheme Proposals

As previously mentioned, the use of an infiltration system to discharge surface water flows from the development is unlikely to be viable, therefore, we would advocate a separate surface water drainage system, with an outfall to the existing public combined sewer situated along the southern boundary of the site, should be designed in accordance with all statutory standards. The maximum permissible discharge of surface water drainage from the development site to the public combined sewer will be in the order of 10.2 l/s subject to the approval of DCWW.

The attenuation required on-site to cater for storm up to and including the 1 in 100 year plus climate change event would be in the order of 190m³ based upon storage calculations using MicroDrainage.

It is acknowledged that as part of the detailed design anti-siltation catch-pits and measures will need to be incorporated upstream of the attenuation and flow control device.

Indicative proposals for the surface water drainage are shown on drawing V-R6393 enclosed within Appendix 4.7, with attenuation calculations provided in Appendix 4.8.

3 Recommendations & Conclusions

3.1 Recommendations

If percolation testing is required by DCWW to verify the on-site infiltration potential of the underlying ground to supplement the findings of the ground investigation report we would advocate they are undertaken in accordance with BRE365 guidance.

In the event that infiltration systems are agreed to be unsuitable with DCWW for the disposal of surface water run-off, then a restricted discharge of 10.2l/s via the existing connection to DCWW's public combined drainage system should be pursued and adequate on-site attenuation be provided. This discharge rate and easements should also be agreed with DCWW before the detail design is commenced.

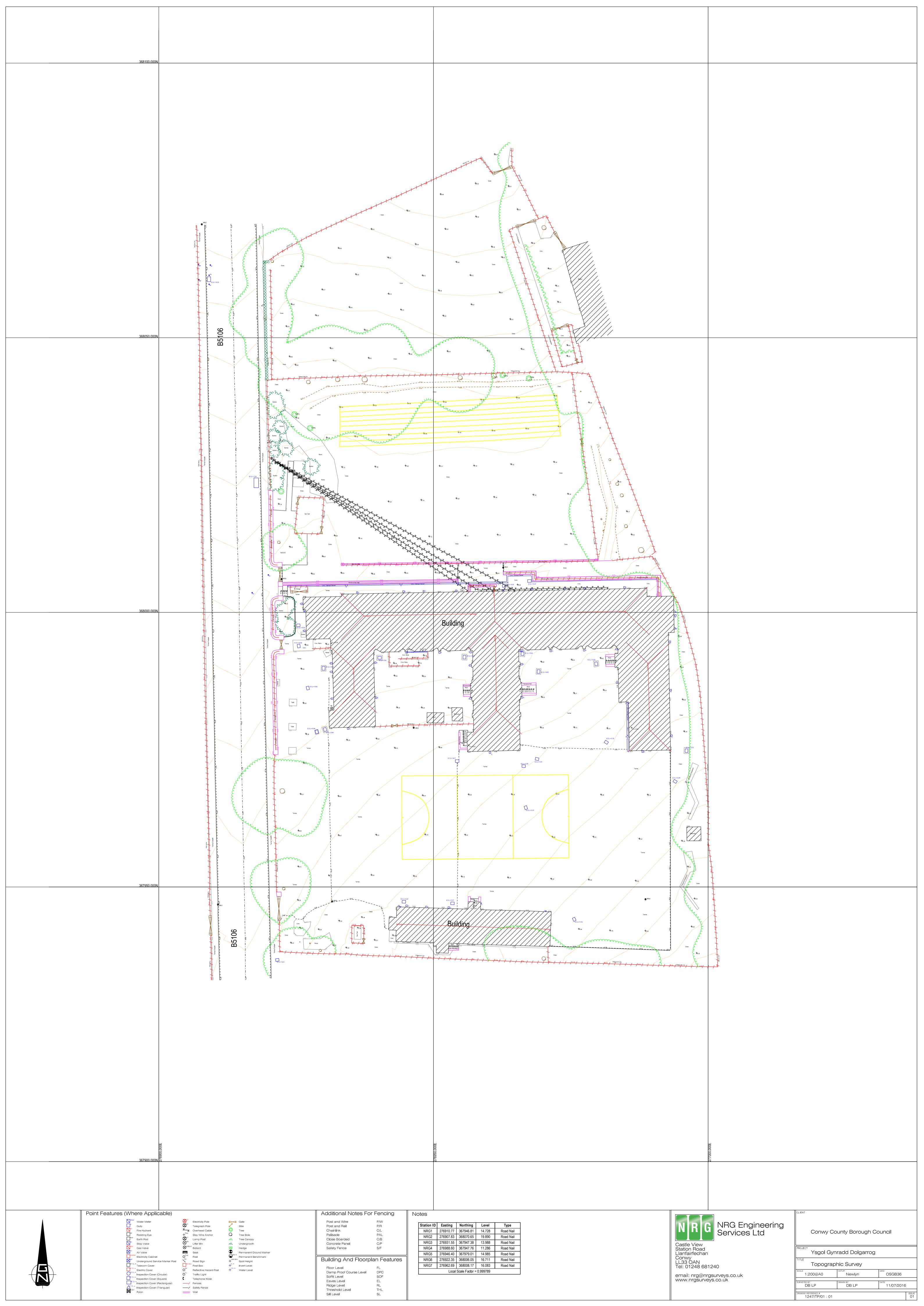
3.2 Conclusions

The proposed site was not found to be at risk of fluvial flood risk and, subject to further surveys and discussions with DCWW, suitable points of connection were identified for the disposal of the foul effluent and surface water run-off generated from the proposed development.

The proposed development is not expected to be affected by general objections in respect to draining the site. There will also be suitable conditions imposed to ensure that the drainage proposals are designed and constructed in accordance with relevant statutory requirements, including Building Regulations 2010 and the requirements of the Local Authority.

4 Appendices

- 4.1 Topographical Survey
- 4.2 Sewer Record Plan
- **4.3** Existing Drainage Survey
- 4.4 NRW Flood Map
- 4.5 Proposed Development Plan
- 4.6 Greenfield Run-off Calculations
- 4.7 Indicative Drainage Layout
- 4.8 Typical Attenuation Volume

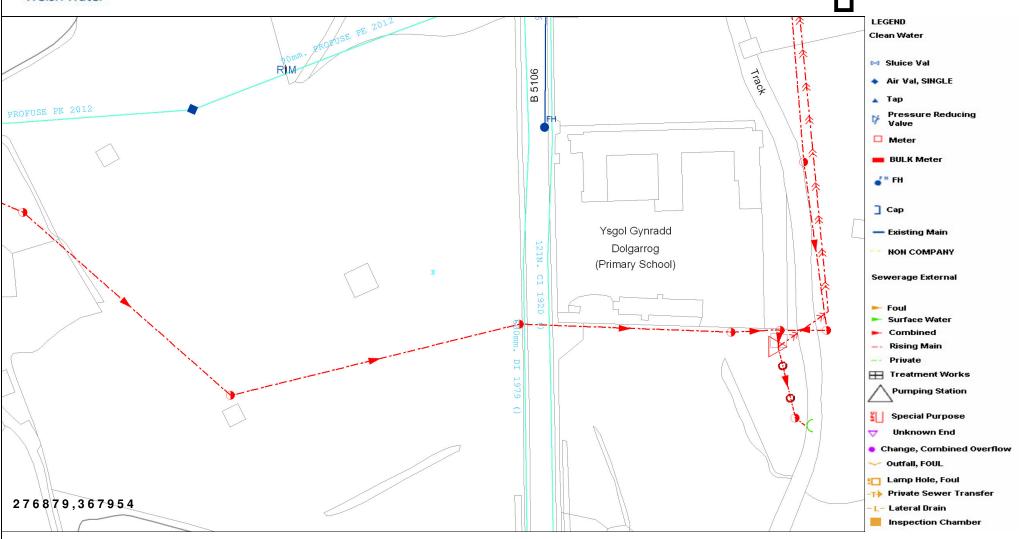




Caerhun Area School



Scale: 1:1250



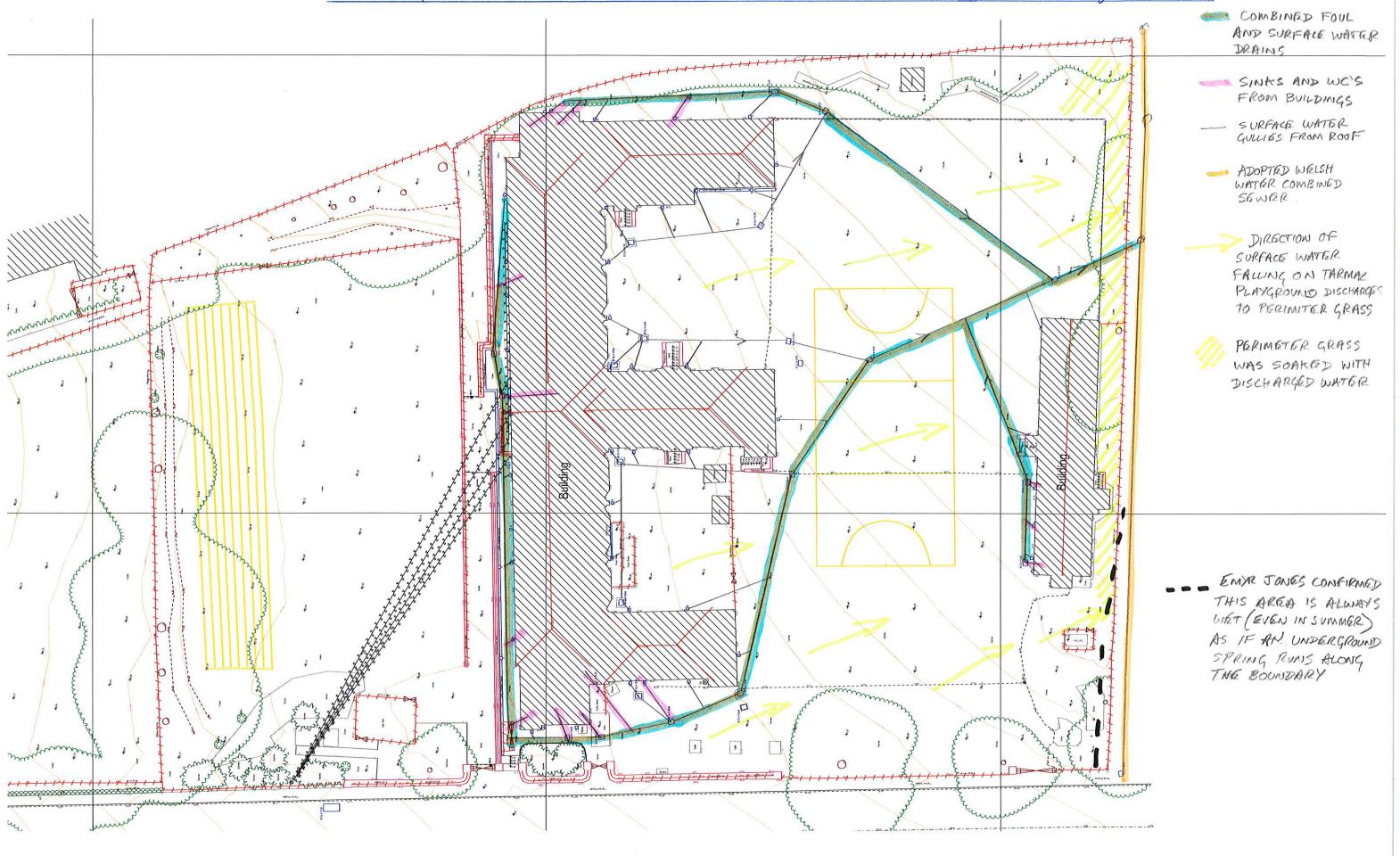
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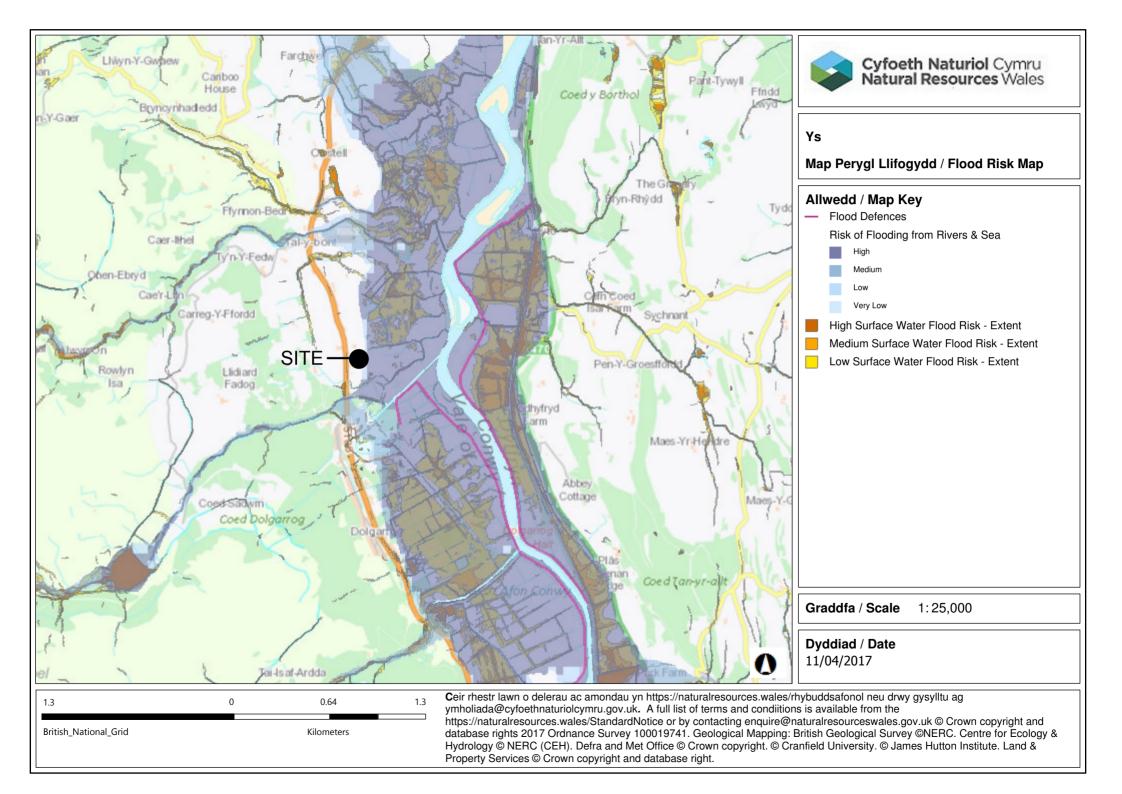
EXACT LOCATION OF ALL APPARATUS TO BE DETERMINED ON SITE

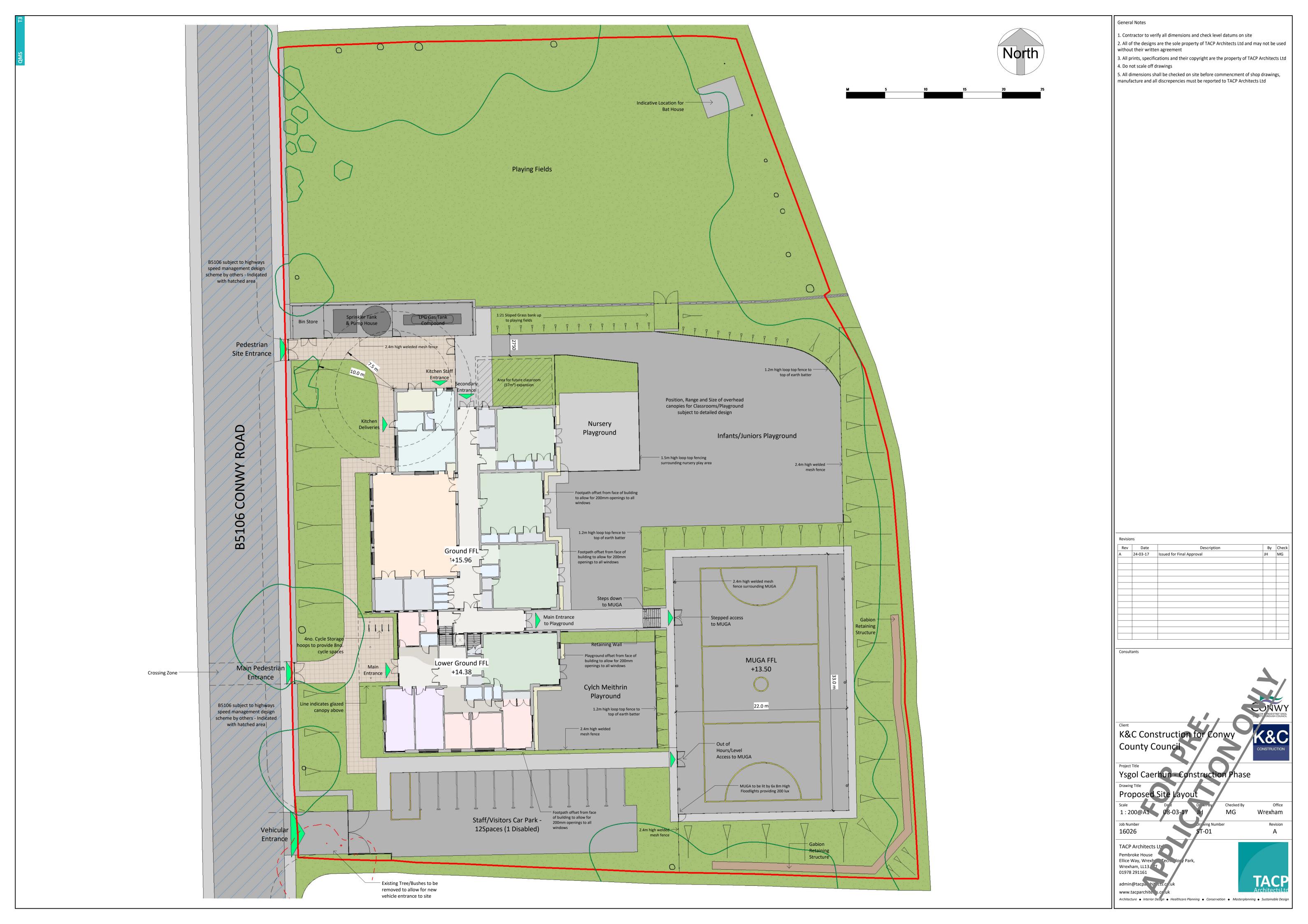
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Reproduced from the Ordnance Whilst every reasonable effort has been Survey's maps with the taken to correctly record the pipe material of DCWW assets, there is a possibility that in some cases pipe material (other than Asbestos Cement or Pitch Fibre) may be found to be asbestos cement (AC) or Pitch Fibre (PF) . It is therefore advisable that the possible presence of AC or PF pipes be anticipated and considered as part of any risk assessment prior to excavation

DOLGARROG SCHOOL - DRAINAGE SURVEY UNDERTAEN ON SITE ON 30/3/17 BETWEEN DWILKINSON (K+C) AND EMYR JONES (CARETAKER)







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ICP SUDS Mean Annual Flood

Input

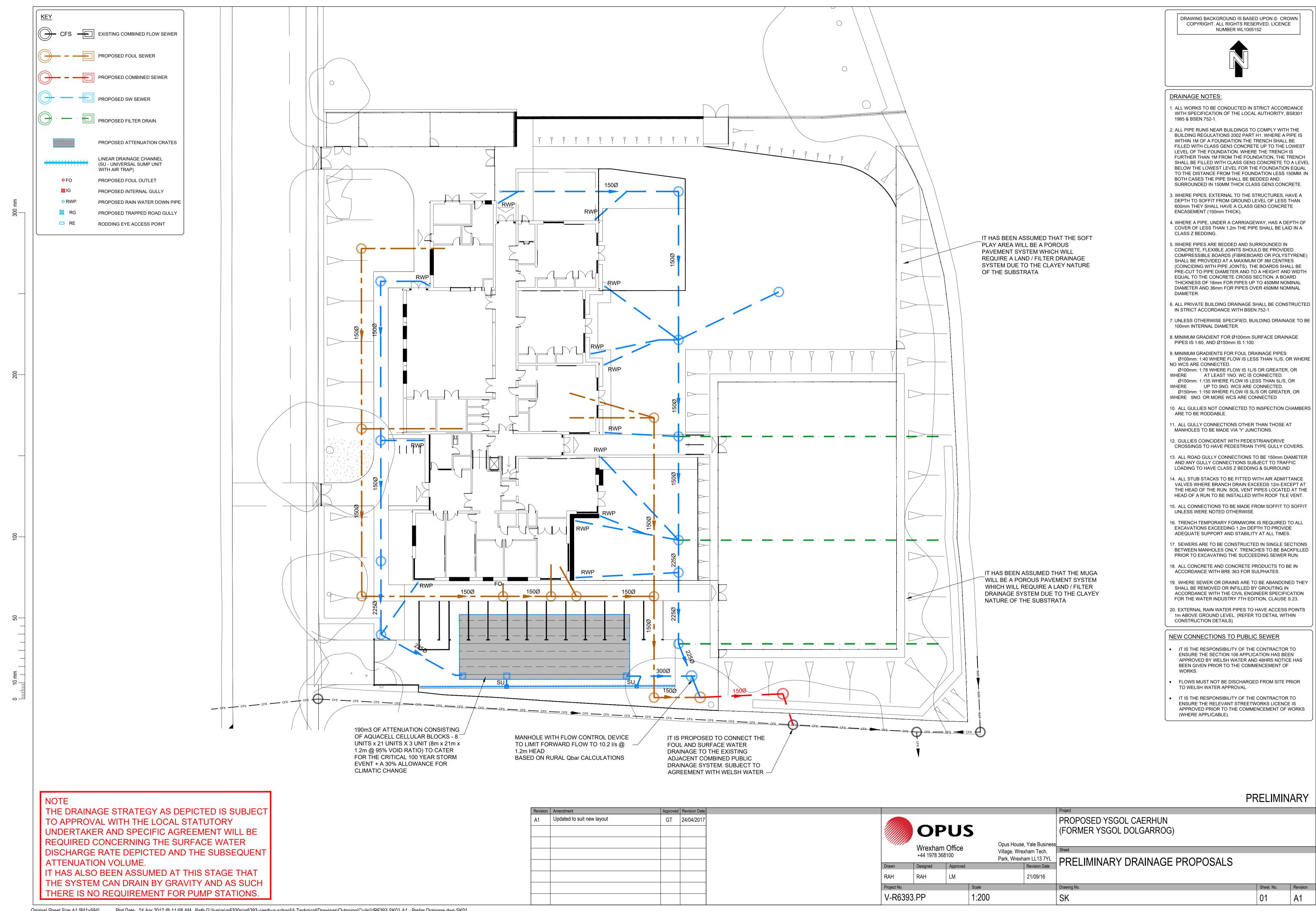
Return Period (years) 1 Soil 0.500 Area (ha) 0.522 Urban 0.000 SAAR (mm) 2083 Region Number Region 9

Results 1/s

QBAR Rural 10.3 QBAR Urban 10.3

Q1 year 9.1

Q1 year 9.1 Q30 years 18.2 Q100 years 22.5



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Summary of Results for 100 year Return Period (+30%)

Half Drain Time : 163 minutes.

Storm		Max	Max	Max	Max	Max	Max	Status
	Event	Level	Depth	Infiltration	Control	Σ Outflow	Volume	
		(m)	(m)	(1/s)	(1/s)	(1/s)	(m³)	
15	min Sum	mer 12.478	0.478	0.0	10.1	10.1	76.3	O K
30	min Sum	mer 12.665	0.665	0.0	10.1	10.1	106.1	O K
60	min Sum	mer 12.852	0.852	0.0	10.1	10.1	135.9	O K
120	min Sum	mer 12.990	0.990	0.0	10.1	10.1	158.0	O K
180	min Sum	mer 13.030	1.030	0.0	10.2	10.2	164.4	O K
240	min Sum	mer 13.038	1.038	0.0	10.3	10.3	165.6	O K
360	min Sum	mer 13.024	1.024	0.0	10.2	10.2	163.5	O K
480	min Sum	mer 12.996	0.996	0.0	10.1	10.1	159.0	O K
600	min Sum	mer 12.962	0.962	0.0	10.1	10.1	153.5	O K
720	min Sum	mer 12.924	0.924	0.0	10.1	10.1	147.4	O K
960	min Sum	mer 12.843	0.843	0.0	10.1	10.1	134.5	O K
1440	min Sum	mer 12.658	0.658	0.0	10.1	10.1	105.1	O K
2160	min Sum	mer 12.403	0.403	0.0	10.1	10.1	64.3	O K
2880	min Sum	mer 12.258	0.258	0.0	10.0	10.0	41.2	O K
4320	min Sum	mer 12.154	0.154	0.0	9.1	9.1	24.6	O K
5760	min Sum	mer 12.128	0.128	0.0	7.5	7.5	20.4	O K
7200	min Sum	mer 12.113	0.113	0.0	6.4	6.4	18.1	O K
8640	min Sum	mer 12.104	0.104	0.0	5.6	5.6	16.5	O K
10080	min Sum	mer 12.097	0.097	0.0	5.0	5.0	15.4	O K
15	min Win	ter 12.541	0.541	0.0	10.1	10.1	86.3	O K

	Stor	m	Rain	Flooded	Discharge	Time-Peak
	Even	t	(mm/hr)	Volume	Volume	(mins)
				(m³)	(m³)	
15	min	Summer	93.473	0.0	84.0	21
30	min	Summer	66.241	0.0	119.3	35
60	min	Summer	44.962	0.0	162.3	6 4
120	min	Summer	29.503	0.0	213.1	120
180	min	Summer	22.662	0.0	245.5	150
240	min	Summer	18.611	0.0	268.9	182
360	min	Summer	14.043	0.0	304.3	250
480	min	Summer	11.489	0.0	332.0	320
600	min	Summer	9.820	0.0	354.7	390
720	min	Summer	8.632	0.0	374.2	460
960	min	Summer	7.032	0.0	406.4	598
1440	min	Summer	5.252	0.0	455.3	866
2160	min	Summer	3.910	0.0	508.6	1196
2880	min	Summer	3.164	0.0	548.8	1532
4320	min	Summer	2.347	0.0	610.6	2204
5760	min	Summer	1.902	0.0	659.8	2936
7200	min	Summer	1.616	0.0	700.8	3672
8640	min	Summer	1.415	0.0	736.5	4400
10080	min	Summer	1.266	0.0	768.4	5128
15	min	Winter	93.473	0.0	94.2	21

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Summary of Results for 100 year Return Period (+30%)

	Storm Event		Max Level (m)	Max Depth (m)	Max Infiltration (1/s)	Max Control (1/s)	Max Σ Outflow (1/s)	Max Volume (m³)	Status
30	min N	Winter	12.753	0.753	0.0	10.1	10.1	120.3	ОК
			12.967		0.0	10.1		154.4	0 K
			13.139		0.0	10.7	10.7	181.8	ОК
180	min V	Winter	13.183	1.183	0.0	10.9	10.9	188.9	ОК
240	min V	Winter	13.189	1.189	0.0	10.9	10.9	189.8	ОК
360	min V	Winter	13.163	1.163	0.0	10.8	10.8	185.7	ОК
480	min V	Winter	13.114	1.114	0.0	10.6	10.6	177.8	O K
600	min V	Winter	13.054	1.054	0.0	10.3	10.3	168.3	O K
720	min V	Winter	12.991	0.991	0.0	10.1	10.1	158.2	O K
960	min V	Winter	12.860	0.860	0.0	10.1	10.1	137.2	O K
1440	min V	Winter	12.538	0.538	0.0	10.1	10.1	85.9	O K
2160	min V	Winter	12.236	0.236	0.0	10.0	10.0	37.6	O K
2880	min V	Winter	12.151	0.151	0.0	8.9	8.9	24.1	O K
4320	min V	Winter	12.117	0.117	0.0	6.7	6.7	18.7	O K
5760	min V	Winter	12.102	0.102	0.0	5.4	5.4	16.2	O K
7200	min V	Winter	12.092	0.092	0.0	4.6	4.6	14.6	O K
8640	min V	Winter	12.085	0.085	0.0	4.0	4.0	13.5	O K
0800	min V	Winter	12.079	0.079	0.0	3.6	3.6	12.6	O K

Storm			Rain	Flooded	Discharge	Time-Peak
	Even	t	(mm/hr)	Volume	Volume	(mins)
				(m³)	(m³)	
30	min	Winter	66.241	0.0	133.6	35
60	min	Winter	44.962	0.0	181.8	62
120	min	Winter	29.503	0.0	238.7	118
180	min	Winter	22.662	0.0	275.0	168
240	min	Winter	18.611	0.0	301.2	192
360	min	Winter	14.043	0.0	340.9	270
480	min	Winter	11.489	0.0	371.9	346
600	min	Winter	9.820	0.0	397.3	422
720	min	Winter	8.632	0.0	419.1	496
960	min	Winter	7.032	0.0	455.2	644
1440	min	Winter	5.252	0.0	510.0	898
2160	min	Winter	3.910	0.0	569.7	1192
2880	min	Winter	3.164	0.0	614.7	1476
4320	min	Winter	2.347	0.0	683.9	2204
5760	min	Winter	1.902	0.0	739.0	2920
7200	min	Winter	1.616	0.0	784.9	3616
8640	min	Winter	1.415	0.0	824.9	4320
10080	min	Winter	1.266	0.0	860.7	5064

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Model Details

Storage is Online Cover Level (m) 13.500

Cellular Storage Structure

Invert Level (m) 12.000 Safety Factor 2.0 Infiltration Coefficient Base (m/hr) 0.00000 Porosity 0.95 Infiltration Coefficient Side (m/hr) 0.00000

Depth (m) Area	(m²)	Inf.	Area	(m²)	Depth	(m)	Area	(m²)	Inf.	Area	(m²)
0.0	00 1	168.0			0.0	1.	.201		0.0			0.0
1.2	00 1	68.0			0.0							

Hydro-Brake Optimum® Outflow Control

Unit Reference MD-SHE-0146-1010-1000-1010 1.000 Design Head (m) Design Flow (1/s) 10.1 Flush-Flo™ Calculated Objective Minimise upstream storage Diameter (mm) 12.000 Invert Level (m) 225 Minimum Outlet Pipe Diameter (mm) Suggested Manhole Diameter (mm) 1200

Control Points	Head (m)	Flow (1/s)
Design Point (Calculated)	1.000	10.1
Flush-Flo™	0.304	10.1
Kick-Flo®	0.674	8.4
Mean Flow over Head Range	-	8.6

The hydrological calculations have been based on the ${\tt Head/Discharge}$ relationship for the Hydro-Brake Optimum® as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m) Flo	w (1/s)	Depth (m) Flow	(1/s)	Depth (m) Flow	(1/s)	Depth (m)	Flow (1/s)
0.100	5.3	1.200	11.0	3.000	17.0	7.000	25.5
0.200	9.8	1.400	11.8	3.500	18.3	7.500	26.3
0.300	10.1	1.600	12.6	4.000	19.5	8.000	27.2
0.400	9.9	1.800	13.3	4.500	20.6	8.500	28.0
0.500	9.7	2.000	14.0	5.000	21.7	9.000	28.8
0.600	9.2	2.200	14.6	5.500	22.7	9.500	29.5
0.800	9.1	2.400	15.3	6.000	23.7		
1.000	10.1	2.600	15.9	6.500	24.6		

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